

무봉산 자율운전 소형원자로용 $\text{UO}_2\text{-U}_3\text{Si}_2$ 복합 핵연료

안 상준*

울산과학기술원 | 원자력공학과 | 핵연료및재료연구실

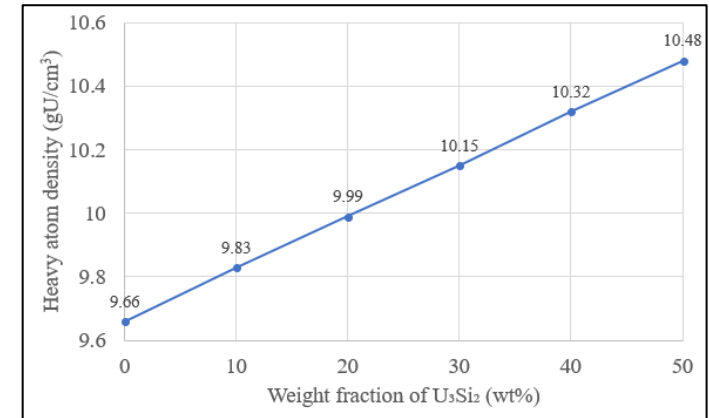
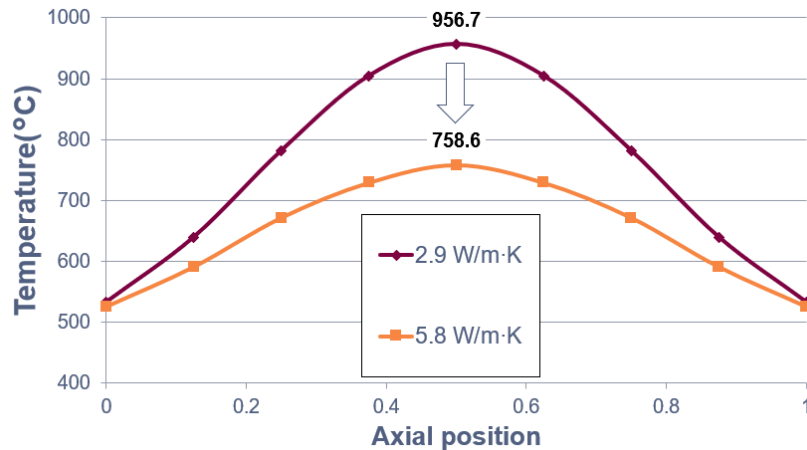
2022. 5. 18.

Contents

1. Background
2. $\text{UO}_2\text{-U}_3\text{Si}_2$ pellet fabrication
3. Thermal conductivity measurement
4. Oxidation resistance
5. $\text{UO}_2\text{-U}_3\text{Si}_2/\text{CSBA}$ fabrication

High thermal conductivity fuel for an advanced SMR

- ❖ To achieve **autonomous boron-free load-following operation**
 - Low T fuel is required → high thermal conductivity fuel is needed.
- ❖ Strategy to achieve '*high k*' fuel w/o decreasing fissile density & oxidation resistance
 - UO_2 -based *high k* ceramics: $\text{UO}_2 + \text{U}_3\text{Si}_2$ or UN
 - SPS(Spark Plasma Sintering): High density & fast sintering



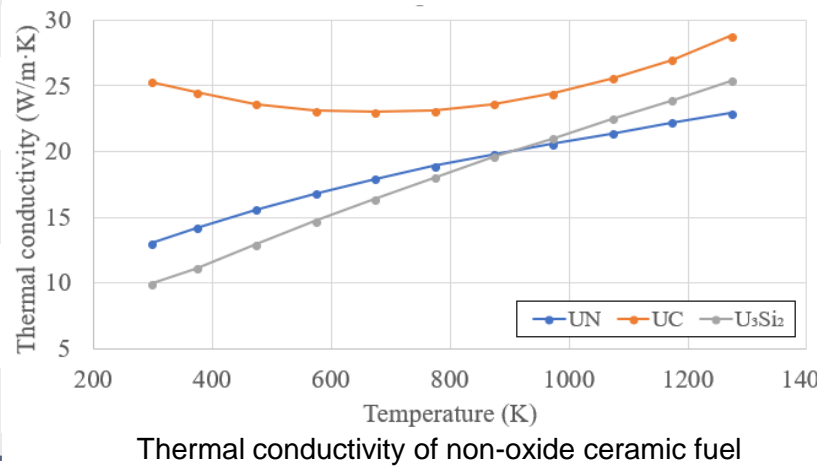
Fissile density increase with U_3Si_2 composition of UO_2 - U_3Si_2 composite pellet

Ab-initio calculation of fuel temperature with fuel thermal conductivity

Background

Additives for UO_2 -based *high k ceramic*

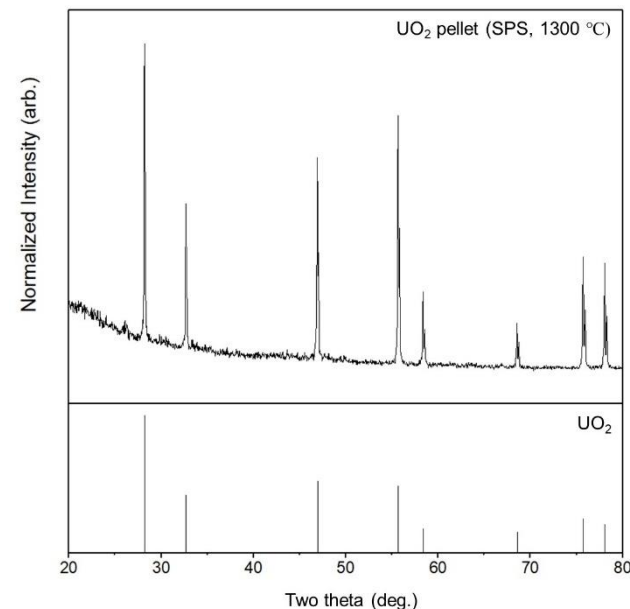
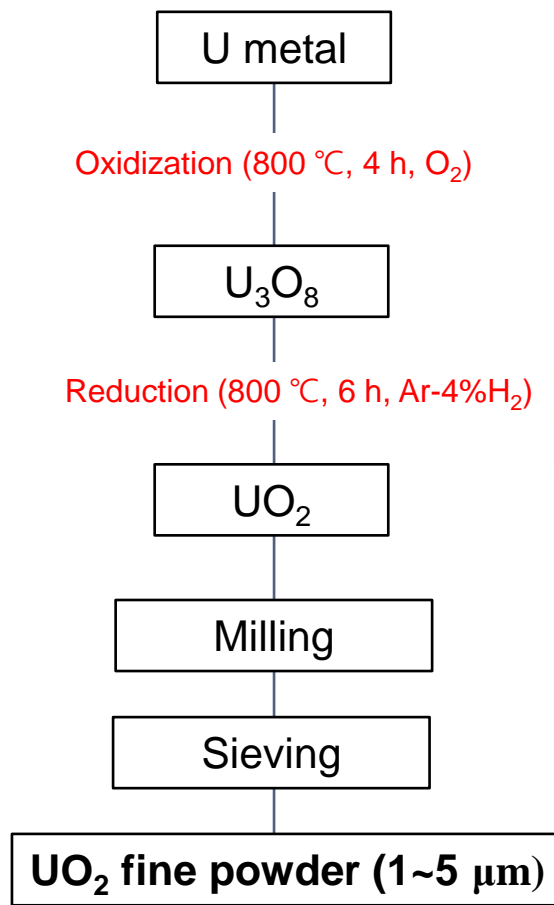
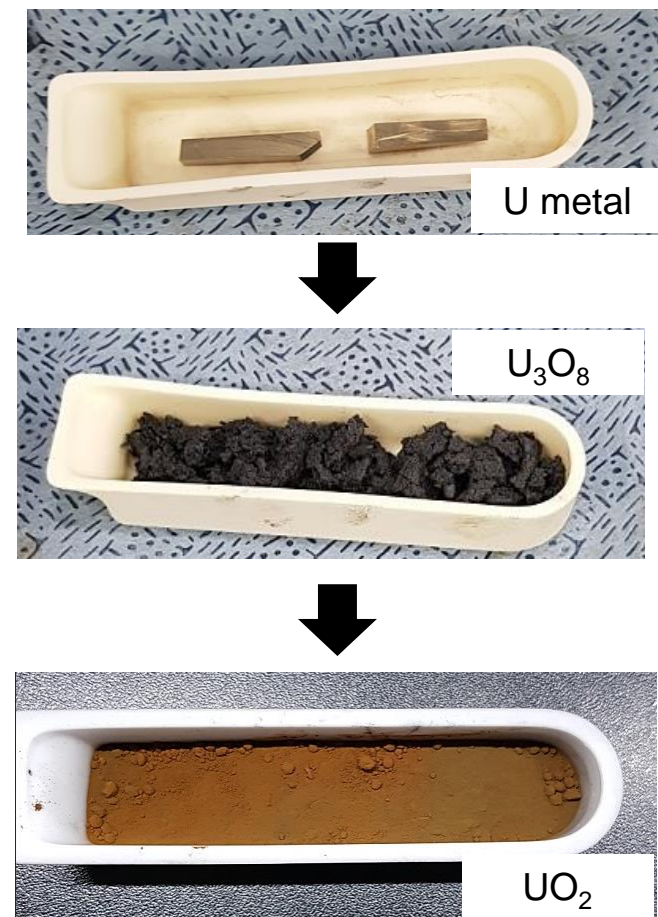
Fuel	UO_2	UC	UN	U_3Si_2
Density (g/cm ³)	10.96	13.6	14.3	12.2
Heavy atom density (gU/cm ³)	9.66	12.9	13.5	11.31
Melting point (°C)	2865	2350	2850	1665
Thermal conductivity at 1000 °C (W/m·K)	2.9	28.8	22.9	25.4
Compatibility with H ₂ O	Very good	Bad	Bad	Average



U_3Si_2 as the material to be tested due to;

- 1. High thermal conductivity
- 2. High fissile density
- 3. Acceptable oxidation resistance
- 4. Fabrication experience as fuel for research reactor

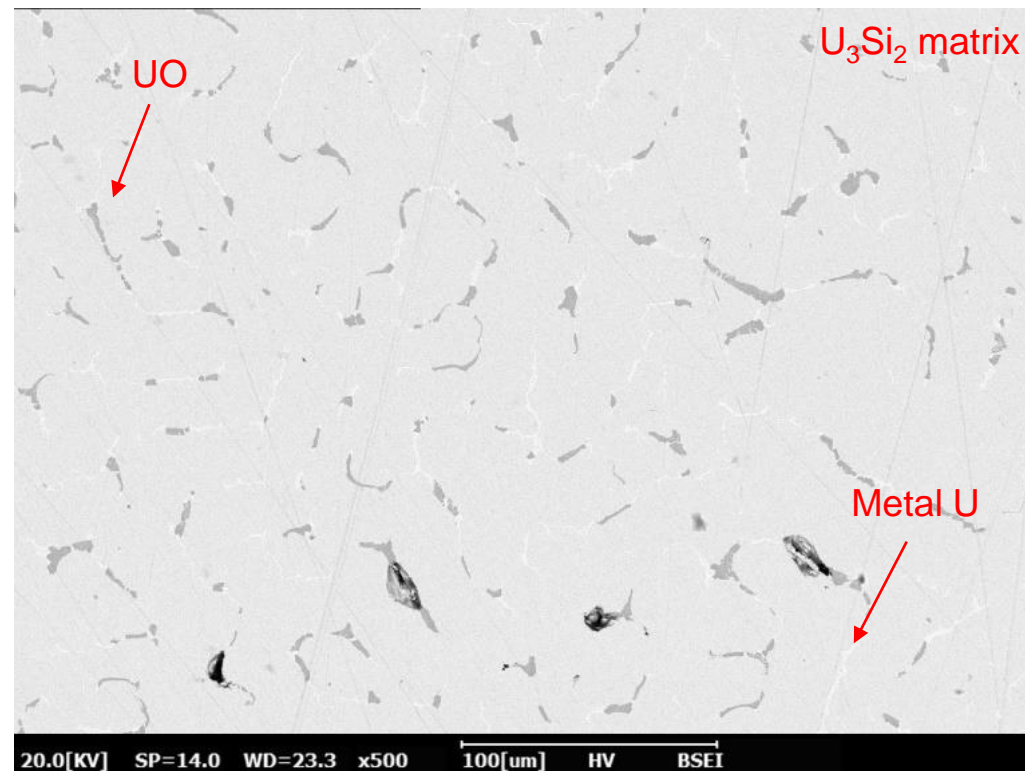
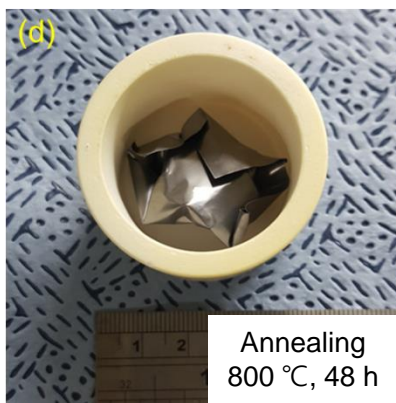
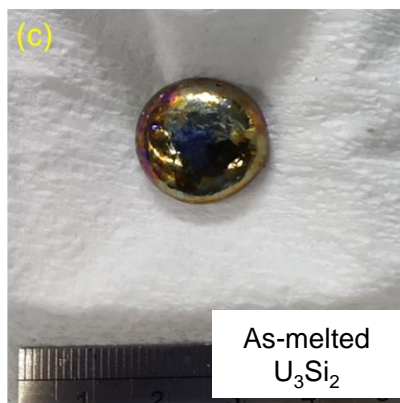
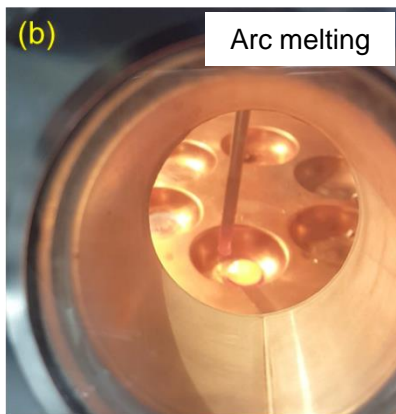
UO₂ powder preparation



XRD analysis on UO₂ pellet

U_3Si_2 synthesis from U and Si powder

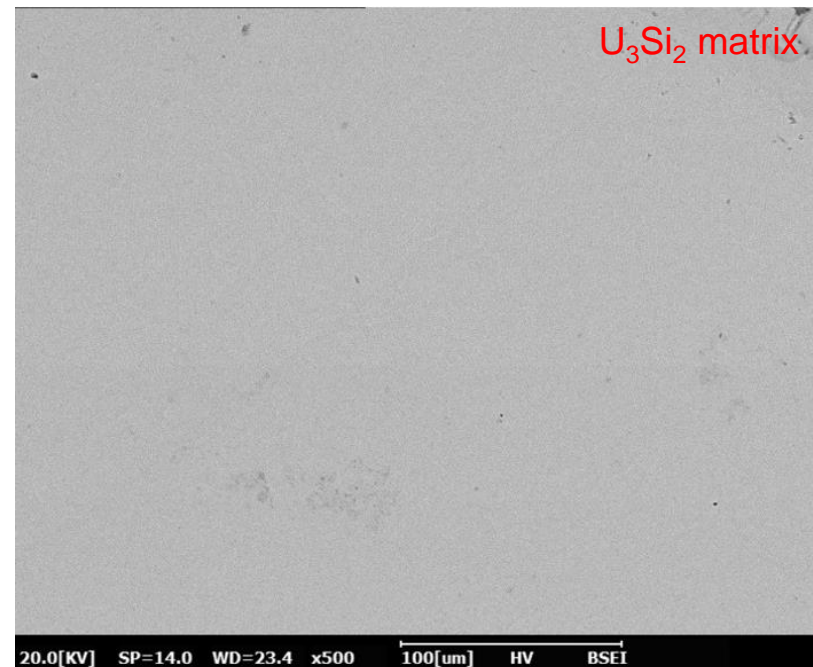
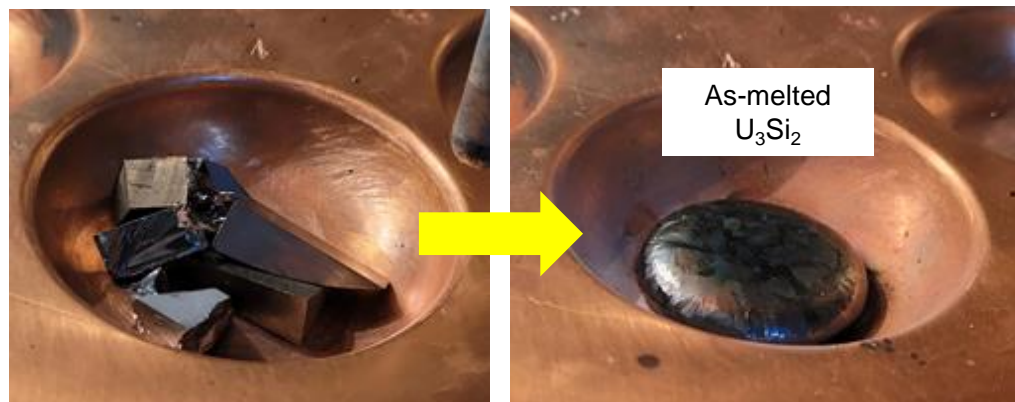
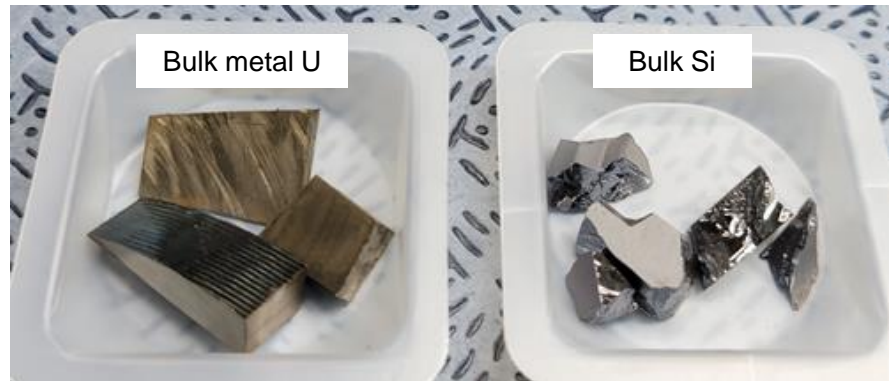
❖ **Oxidation** occurred during process and **metal uranium** phase identified



SEM BSE image of as-melted U_3Si_2

U_3Si_2 synthesis from bulk U and Si

❖ No oxidation and 2nd phase formation



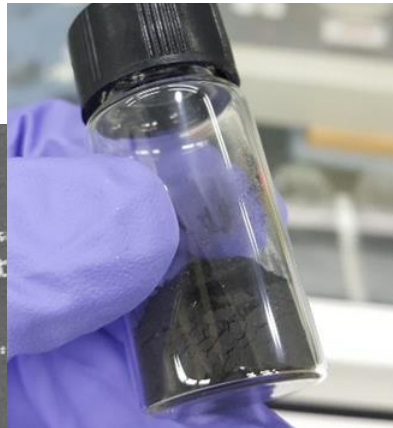
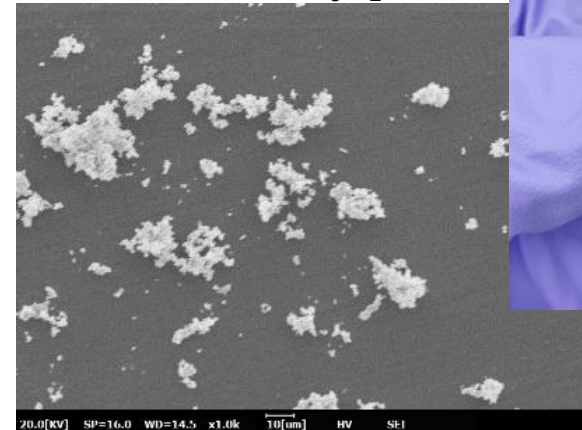
SEM BSE image of as-melted U_3Si_2

U_3Si_2 pulverization and spark plasma sintering

❖ U_3Si_2 pulverization by milling

- Milling at 450 rpm, 8 h, Ar atm.
- **Additional annealing** to as-milled U_3Si_2 powder to remove accumulated strain during milling
 - Annealing at 800 °C, 12 h

SEM-BSE image on U_3Si_2 powder



U_3Si_2 powder

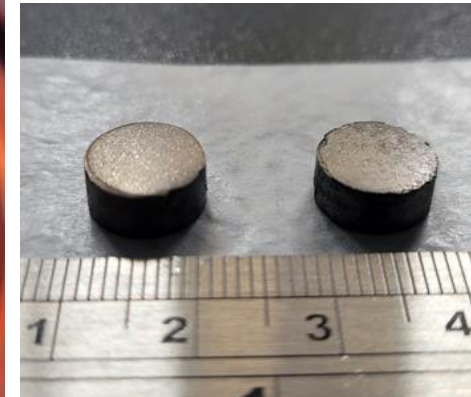
❖ Pellet fabrication through SPS (Spark Plasma Sintering)

- SPS: advanced sintering technique using DC pulse current
- Sintering at 1300 °C, 10 min, vacuum

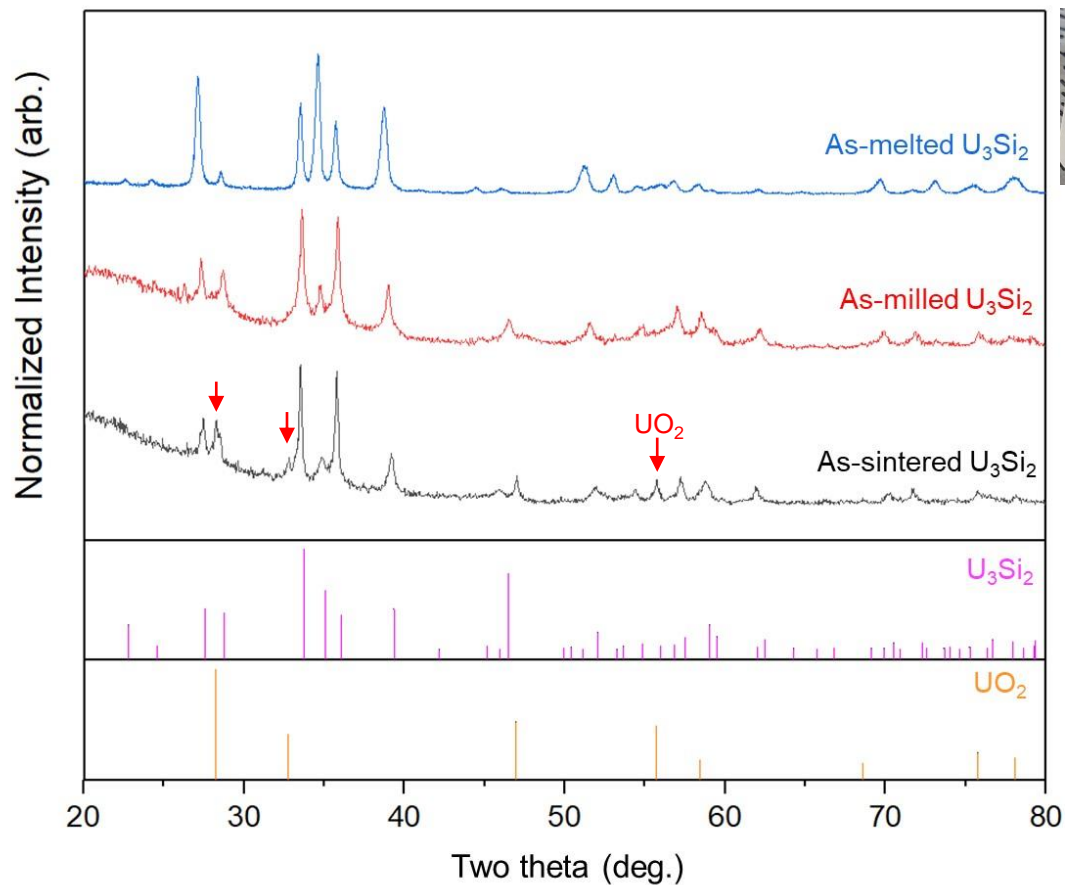


Spark plasma sintering on U_3Si_2 powder

U_3Si_2 pellet (93–95%TD)



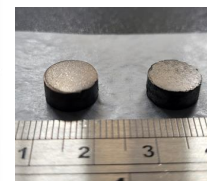
XRD analysis on each powder metallurgy process



Bulk U_3Si_2



Powder
 U_3Si_2



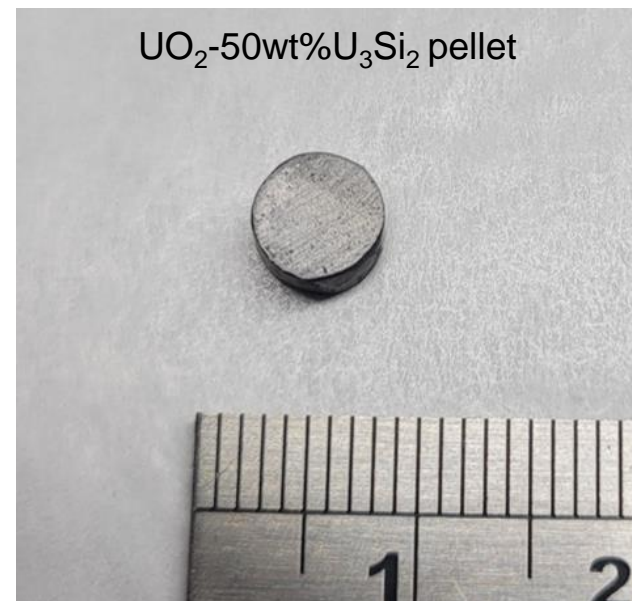
U_3Si_2 pellet

UO_2 - U_3Si_2 composite pellet fabrication using SPS

- ❖ Blending UO_2 and U_3Si_2 powder using 3d mixer.
- ❖ SPS with various silicide composition and sintering temperature.
 - Sintering pressure (20 MPa) and dwell time (10 min) are fixed.

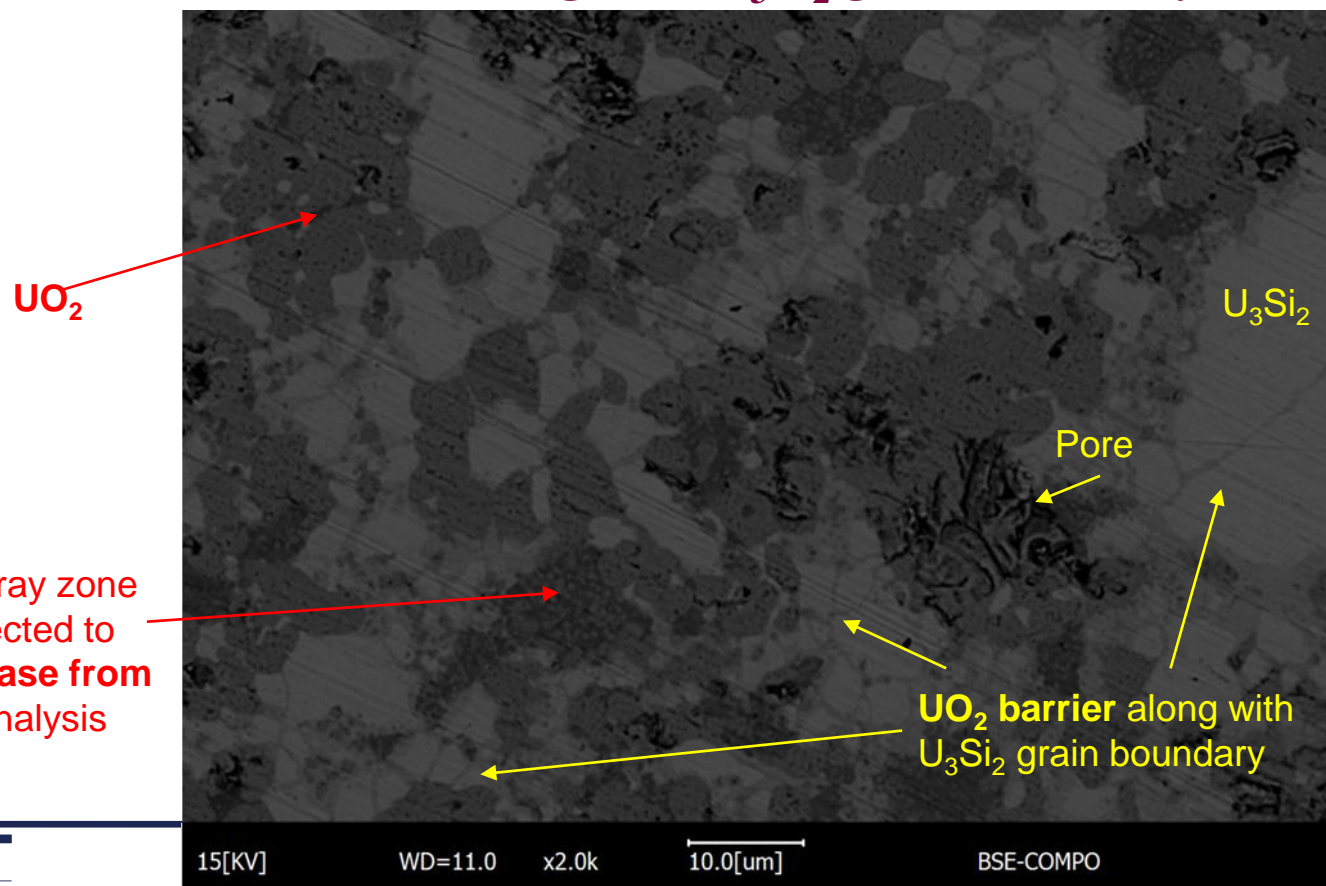
Sample	U_3Si_2 composition (wt%)	Sintering temperature (°C)	Sintered density (g/cm ³)
1	10	1400	9.62
2	30	1400	10.08
3	50	1400	10.18
4	50	1200	9.53
5	50	1000	7.27

*Theoretical density of UO_2 : 10.96 g/cm³
 U_3Si_2 : 11.32 g/cm³



Micrograph analysis on UO₂-50wt%U₃Si₂ pellet

- ❖ **UO phase formation** during sintering.
- ❖ **UO₂ barrier** was formed along with U₃Si₂ grain boundary.



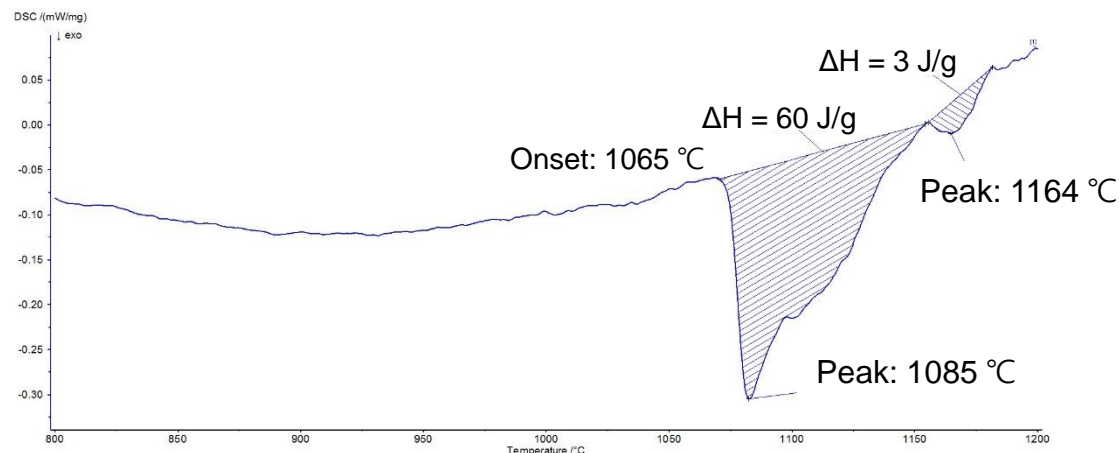
2nd phase formation during SPS of UO₂-U₃Si₂

❖ XRD analysis on UO₂-50wt%U₃Si₂ sintered pellet

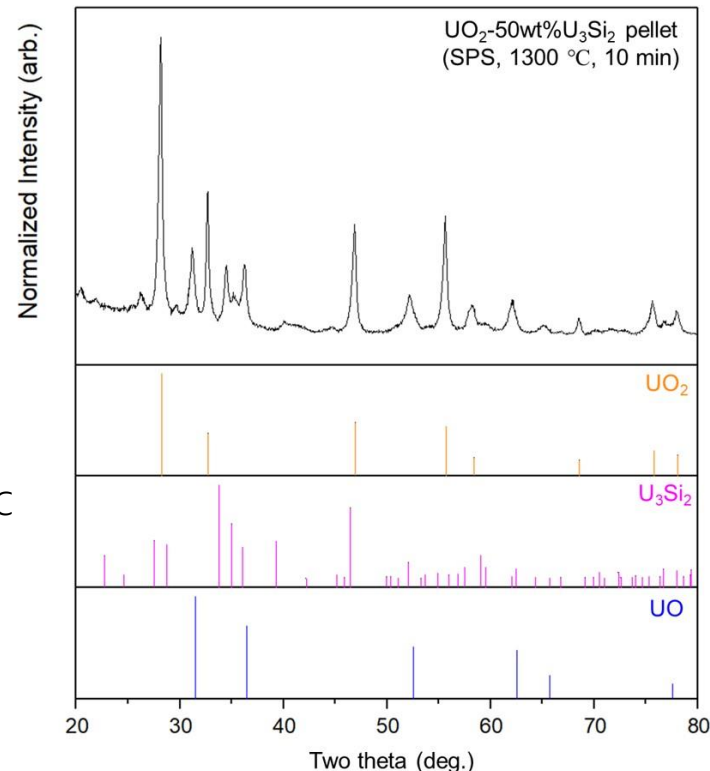
- Showed secondary **UO** phase peak.

❖ DSC analysis on UO₂ and U₃Si₂ powder

- Revealed **exothermal reaction** occurred.
 - From 1050 °C to 1200 °C.

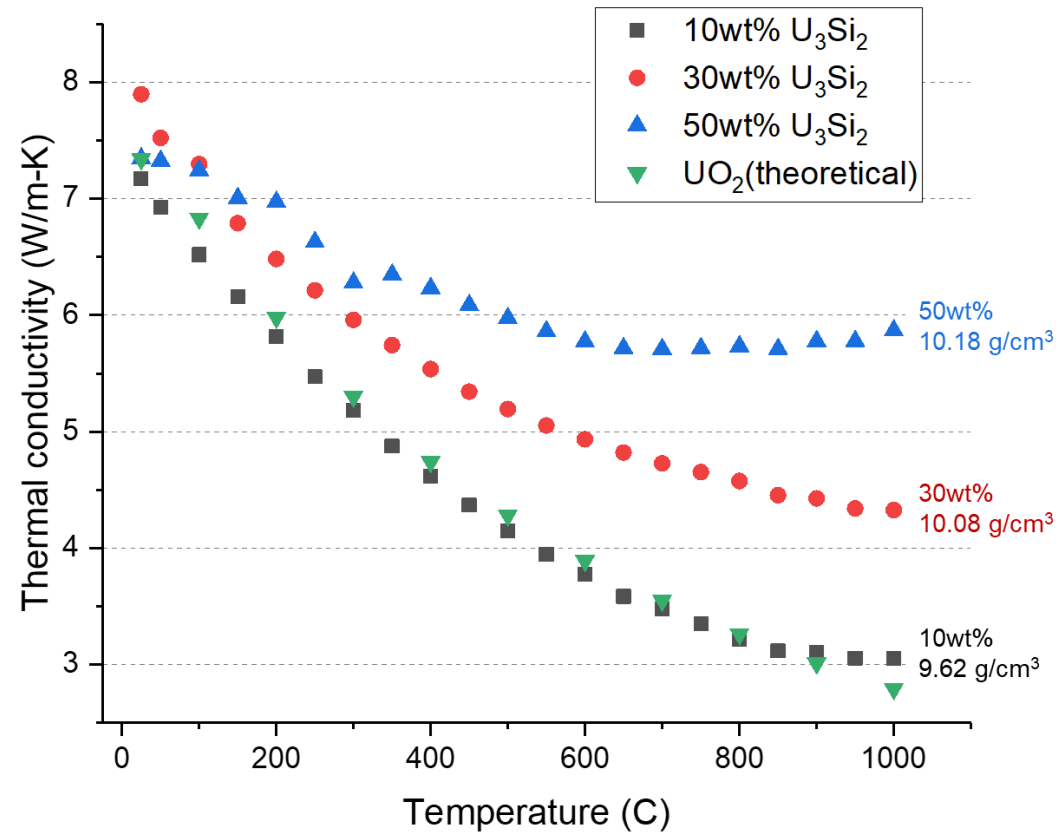


DSC analysis on UO₂-U₃Si₂ mixed powder up to 1200 °C

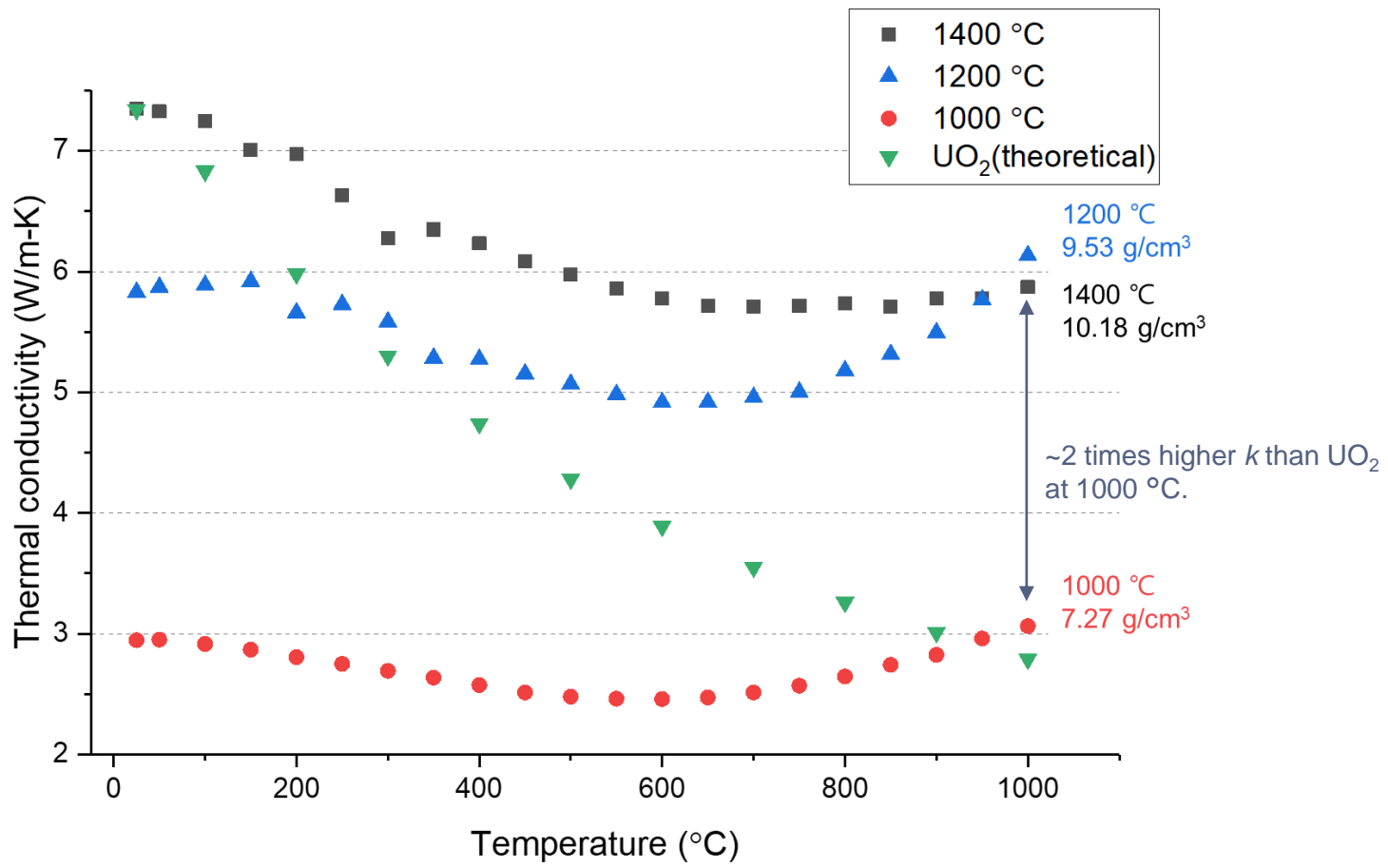


XRD analysis on UO₂-50wt%U₃Si₂ pellet
SPSed at 1400 °C for 10 min

k of $\text{UO}_2\text{-U}_3\text{Si}_2$ pellet as U_3Si_2 composition

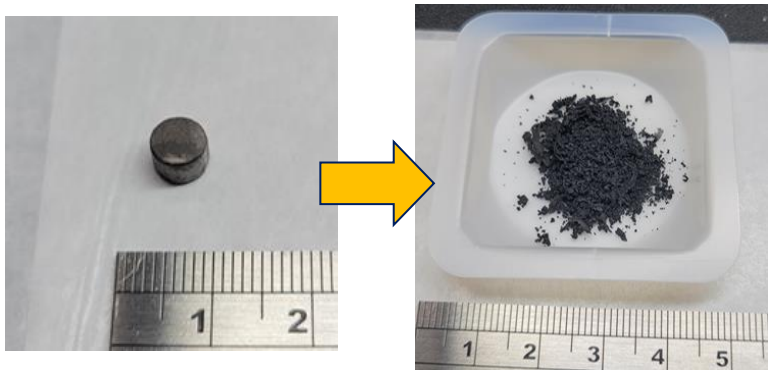


k of $\text{UO}_2\text{-U}_3\text{Si}_2$ pellet as sintering temperature

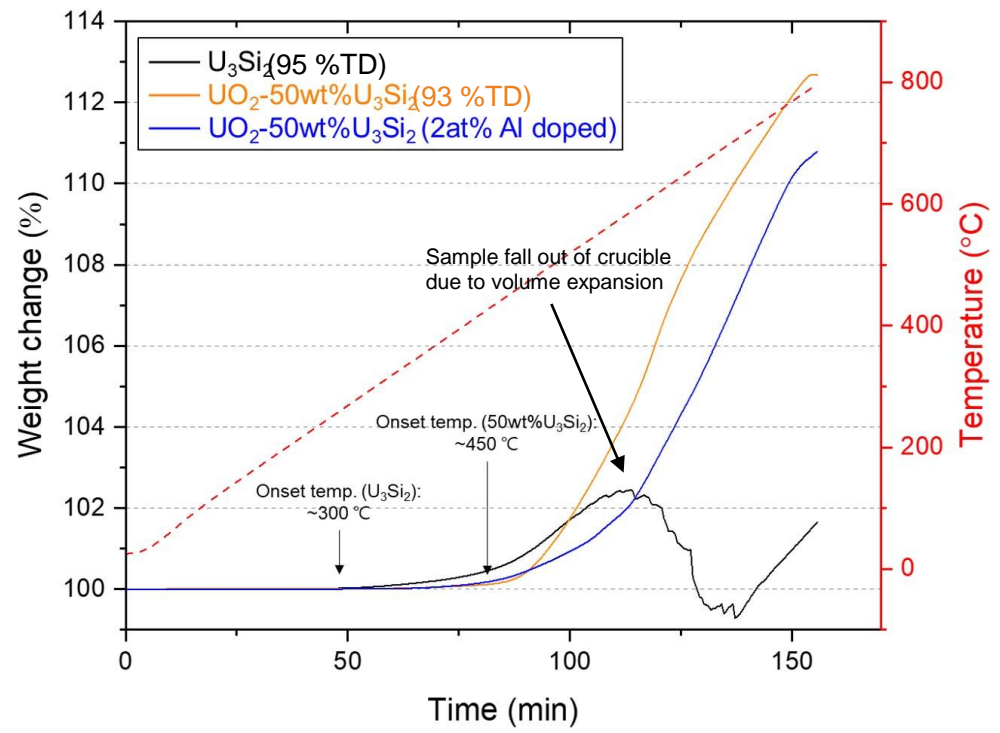


Oxidation resistance of $\text{UO}_2\text{-U}_3\text{Si}_2$ pellet (air)

- ❖ **Ramped temperature oxidation**
 - 5 °C/min, up to 800 °C, air
- ❖ **$\text{UO}_2\text{-U}_3\text{Si}_2$ composite pellet**
 - Increased onset temperature of breakaway oxidation than U_3Si_2 .
- ❖ **Al doping also enhanced oxidation resistance.**



Pulverization of U_3Si_2 during oxidation test



Thermogravimetric analysis (TGA) on UO_2 , $\text{UO}_2\text{-U}_3\text{Si}_2$, and $\text{UO}_2\text{-U}_3\text{Si}_2\text{-Al}$ pellets

Corrosion resistance of $\text{UO}_2\text{-U}_3\text{Si}_2$ pellet (pressurized water)

- ❖ **Enhanced corrosion resistance of $\text{UO}_2\text{-U}_3\text{Si}_2$ than U_3Si_2**
- ❖ **Corrosion test at 300 °C for 24 h under 100 bar H_2O**
 - UO_2 : no corrosion occurred
 - U_3Si_2 : U_4O_9 formation and dissolution
 - $\text{UO}_2\text{-50wt}\%\text{U}_3\text{Si}_2$: no corrosion occurred



Reaction vessel



UO_2



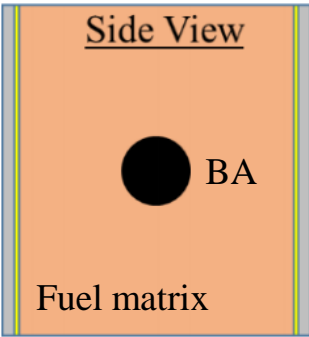
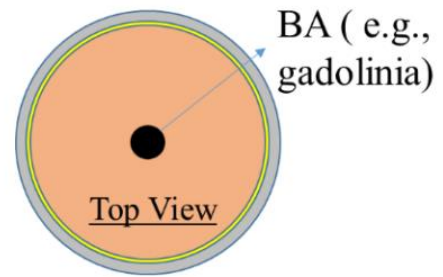
U_3Si_2



$\text{UO}_2\text{-50wt}\%\text{U}_3\text{Si}_2$

Central Shielded Burnable Absorber (CSBA)

- ❖ Conceptually innovative BA design introduced to eliminate the soluble boron.
- ❖ Gd₂O₃ ball fabrication: Drip casting → Drying → Sintering (~89%TD ball)

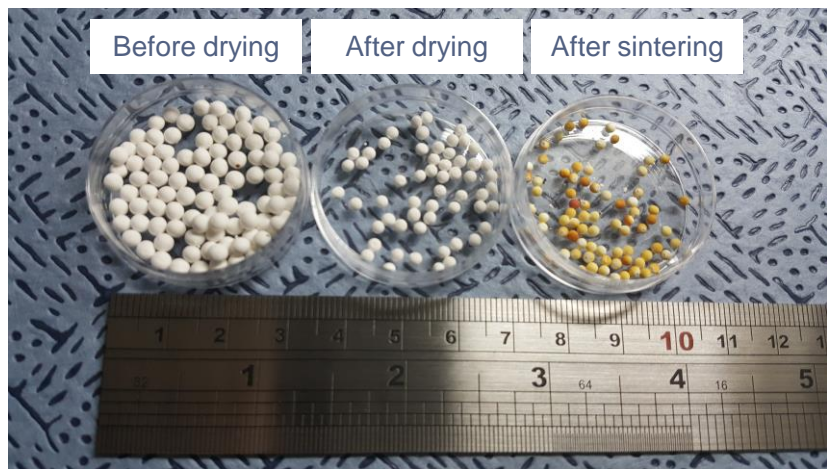


Design of CSBA fuel

Nguyen et al.

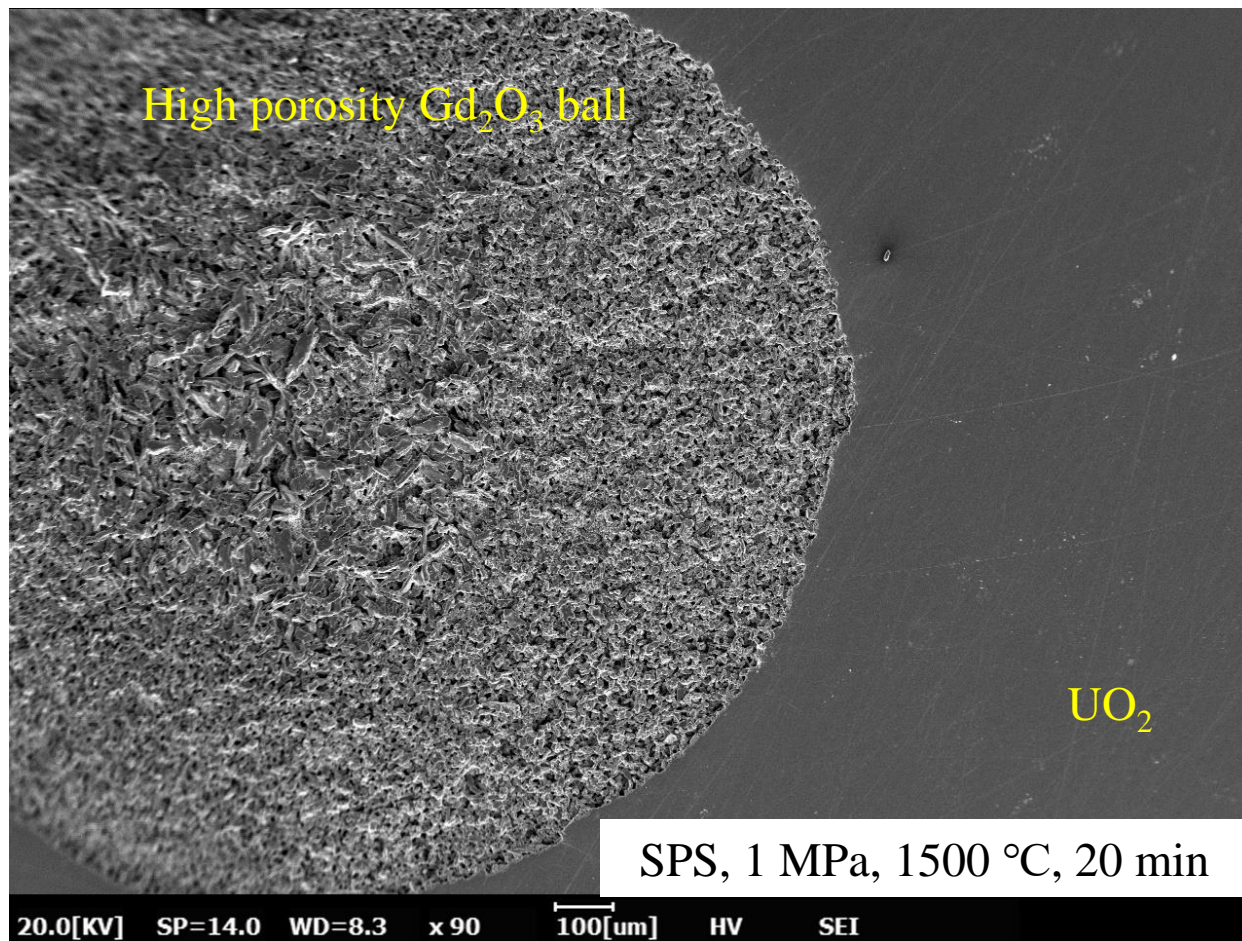
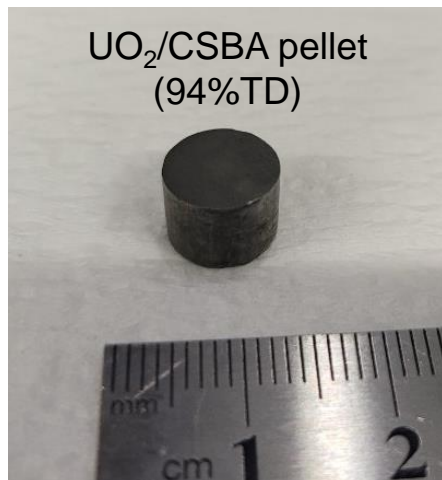


Gd₂O₃ ball drip casting



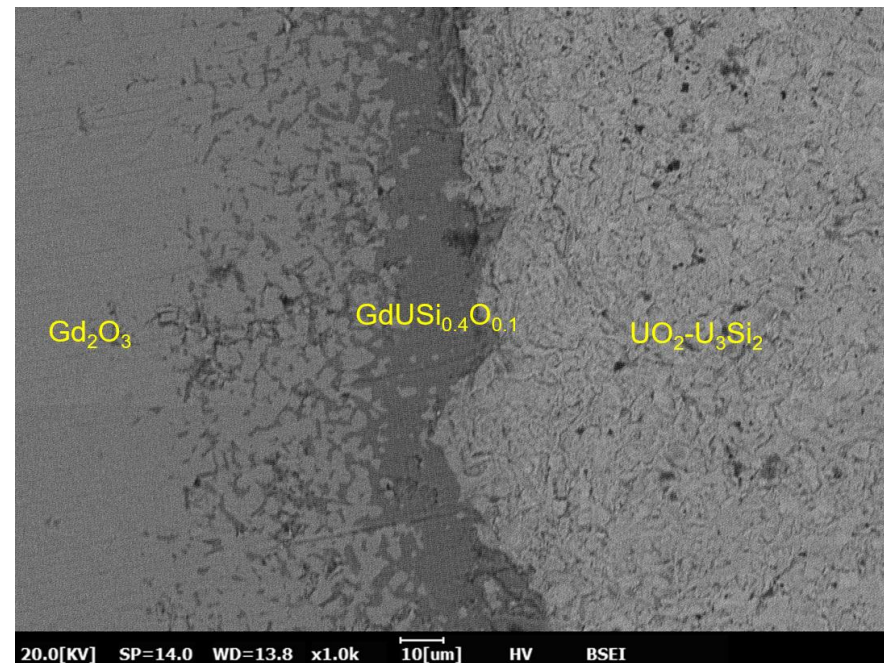
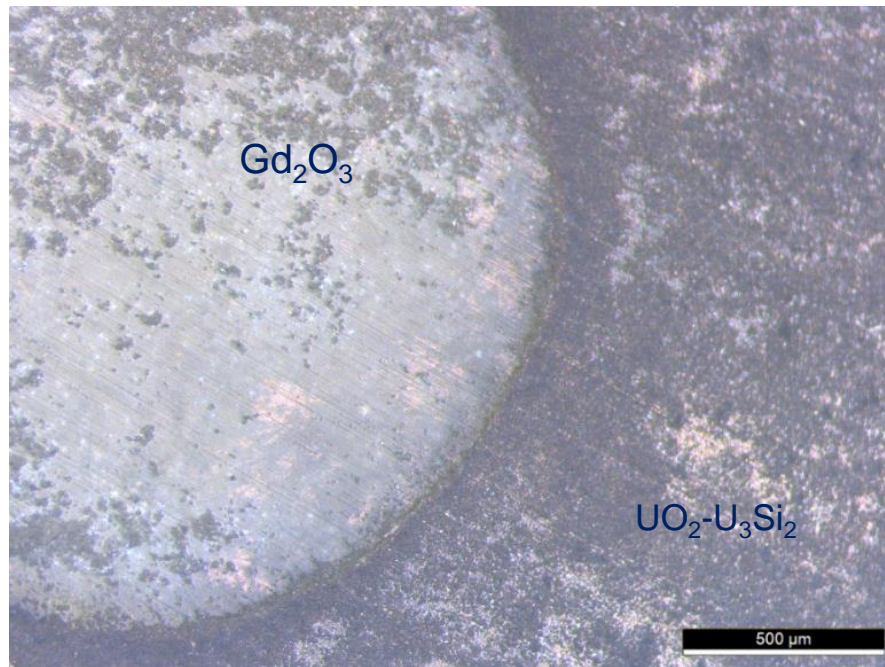
Gd₂O₃ ball sintering

UO_2 /CSBA pellet fabrication (using SPS)



UO_2 - U_3Si_2 /CSBA pellet thermal stress resistance

- ❖ Load following operation → thermal cycle on fuel → **thermal stress**
- ❖ Thermal cycle test on UO_2 - U_3Si_2 /CSBA pellet
 - 600~800 °C, 10 cycle, 200 min/cycle
 - **Interaction layer** observed but **no crack** formed for both Gd_2O_3 ball and UO_2 - U_3Si_2 .



Summary

Summary

Background

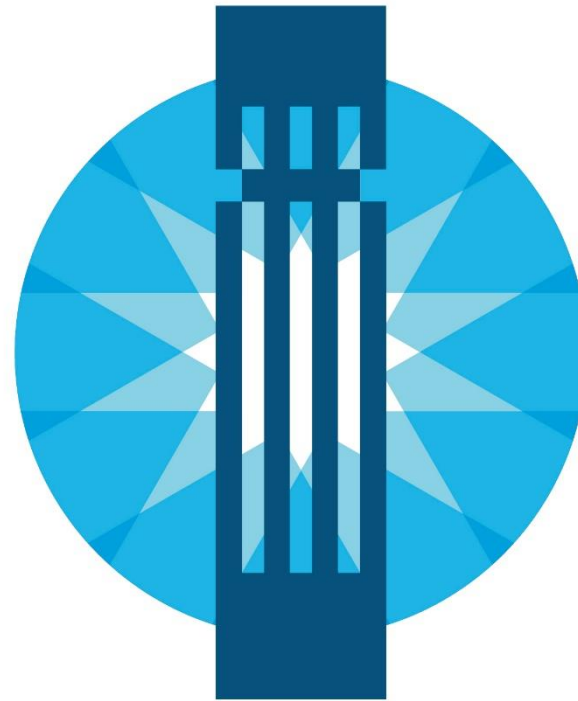
Composite pellet fabrication

Thermal conductivity measurement

Oxidation resistance

UO₂-U₃Si₂/CSBA

- Lower fuel temperature to soluble boron free operation & acceptable corrosion resistance
→ High k UO₂-based composite fuel concept
- **Uranium silicide (U₃Si₂)**: high thermal conductivity & fissile density, acceptable corrosion resistance
- **Spark Plasma Sintering** → 91~93% TD UO₂-U₃Si₂ pellet fabrication
- **Secondary phase (UO) formation** by exothermic reaction at 1050~1200 °C
- **UO₂ barrier formation** along with U₃Si₂ grain boundary
- **Increasing thermal conductivity with increasing U₃Si₂ composition**
 - 10wt% U₃Si₂ pellet showed similar thermal conductivity with UO₂.
 - 50wt% U₃Si₂ : **90% thermal conductivity increase at 1000 °C w.r.t. UO₂**
- **Increasing thermal conductivity with increasing sintering temperature**
 - Sintering @1000 °C pellet: very low k due to low sintering density
 - Too high sintering temperature accelerate **2nd phase formation which has low-thermal conductivity.**
- **Enhanced oxidation resistance of UO₂-U₃Si₂ composite pellet (air oxidation)**
 - Increased onset temperature of UO₂-50wt%U₃Si₂ pellet (450 °C) compared to U₃Si₂ (300 °C).
 - **Enhanced corrosion resistance of UO₂-U₃Si₂ composite pellet (pressurized water)**
 - UO₂-50wt%U₃Si₂ pellet showed no dissolution in pressurized water.
- **No crack formation, but 2nd phase layer formation btw. UO₂-U₃Si₂ and Gd₂O₃ boundary.**



URANUM
NUCLEAR FUEL LAB

Thank you for your attention